

DYNAMIC DEGREES OF FREEDOM AND THE THEORY OF PLASTICITY

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The attempts to describe plastic flow within the framework of non-equilibrium thermodynamics can be traced back for long. Non-linear constitutive equations can display plastic properties even in the state of local equilibrium. The yield condition may be built into the entropy function or into the constitutive equations. A theory based on the hypothesis of local equilibrium has a lot of advantages but the properties of the admissible models are not flexible enough to give quantitative account on real materials. The need to describe several kinds of structural materials makes the introduction of dynamic degrees of freedom indispensable. The dynamic degrees of freedom give rise to a number of new problems not present in the classical theories. First of all, their physical meaning is a great challenge. The possible topological structure of the thermodynamic state space is also problematic. Nevertheless, the above problems are living, the advantages worth a lot.

I intend to survey some methods plastic flow can be described by within the framework of irreversible thermodynamics.

1. Systems in local equilibrium.

First a medium is assumed the local state of which is given by the internal energy and the specific volume. For the sake of simplicity, volume changes will not be regarded; the specific volume is rather a parameter than a variable. The balance equation for the internal energy is of the usual form

$$(1) \quad \rho \frac{du}{dt} + \operatorname{div} J_q = t : \dot{d}$$

where ρ is the density; u the specific internal energy; J_q the heat flow; t Cauchy's stress; \dot{d} the strain rate, i.e. the symmetric part of the velocity gradient. The specific entropy is supposed to depend on only the internal energy

$$s = s(u).$$

Here $s(u)$ is the equilibrium entropy function. The balance equation for the entropy reads

$$(2) \quad \rho \frac{ds}{dt} + \operatorname{div} J_s = \sigma_s,$$

where J_s is the entropy flow connected to the heat flow the usual way;

$$J_s = \frac{1}{T} J_q.$$

The entropy production density is

$$(3) \quad \sigma_s = \frac{1}{T} t : \dot{d} + J_q \operatorname{grad} \frac{1}{T}.$$

Not intending to deal with heat conduction, isotherm circumstances are presumed; so the energy dissipation function reduces to

$$(4) \quad T \sigma_s = t : \dot{d}.$$

If Onsager's linear laws were valid the equations of Newtonian fluids would be obtained, which read

$$t = 2\eta \dot{d}.$$

For plastic flow, the conductivity coefficient denoted here by 2η turn to be a function depending on the thermodynamic force \dot{d} . A proper choice for the function leads to a theory of plastic flow. If the function is chosen as

$$2\eta = \frac{k\sqrt{2}}{\sqrt{\dot{d} : \dot{d}}}$$

we arrive at Mises' theory of plasticity. The model obtained this way is the ideally plastic body, the constitutive equation of which has singularity at equilibrium. Nevertheless, the ideally plastic body is suitable for practical applications, the above mentioned singularity is annoying. The constitutive equation of Bingham's body is obtained by taking

$$2\eta = 2\eta_0 + \frac{k\sqrt{2}}{\sqrt{\dot{d} : \dot{d}}}.$$

The singularity is also present. One may suspect that the mentioned theories are only approximations not valid for very slow motions. The linear equations of thermodynamics for media with dynamic degrees of freedom are free of the singularity.

2. The stability of viscoelastic flow.

Next a medium with several dynamic degrees of freedom are discussed. The non-equilibrium state variables are presumed to be of α -type, i.e. they are invariant under time inversion. The balance equation for the internal energy is the same as above. The entropy is very different. The non-equilibrium states are

assumed to be more complicated than the local equilibrium ones, to give account on the non-equilibrium structures developing during irreversible processes, several – say n – sy trace, second order tensors are needed. According to the Morse-lemma, the independent variables may be chosen so that the entropy has the form

$$(5) \quad s = s^e \left(u - \frac{1}{2\rho} \sum_i \alpha_i : \alpha_i \right),$$

where $s^e(u)$ is the equilibrium entropy function. The balance equation of the entropy is equation (2) and the entropy flow is taken in the classical form. The actual expression for the energy dissipation function reads

$$(6) \quad T\sigma_s = t : \overset{\circ}{d} - \sum_i \alpha_i : \overset{\circ}{\alpha}_i.$$

For simplicity, isotherm motion is presumed. Here the small circle above the symbol of a quantity denotes the co-rotational time derivative. The co-rotational time derivative has the advantage that it is a time derivative in a Euclidean frame and it is objective; so it is zero if the change of the quantity is due to rotation. The linear Onsager equations are

$$(7) \quad \begin{aligned} t &= L_{00} \overset{\circ}{d} - \sum_i L_{0i} \alpha_i \\ \overset{\circ}{\alpha}_i &= -L_{0i} \overset{\circ}{d} - L_i \alpha_i. \end{aligned}$$

Here the fact that an orthogonal transformation preserves the form of the entropy transformation preserves the form of the entropy function (5) has been utilized. This way the relaxation of each dynamic variable is independent from any other.

The solutions of the equations are interesting and display complicated behavior. For steady shear flow the viscometric

functions have the forms

$$(8) \quad \begin{aligned} \tau(\chi) &= \frac{L_{00}}{2} \chi + \sum_i \frac{L_{0i} L_i}{2} \frac{\chi}{L_i^2 + \chi^2}; \\ \sigma_1(\chi) &= -\sigma_2(\chi) = \sum_i \frac{L_{oi}}{2} \frac{\chi^2}{L_i^2 + \chi^2}. \end{aligned}$$

Here χ is the rate of shear. The shear stress function may have decreasing sections where the solution is unstable. The graph of the function is shown in figure 1 for a body with one dynamic degree of freedom.

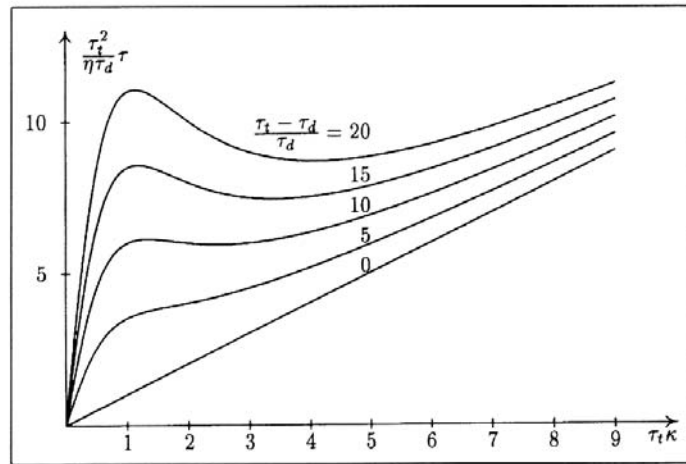


Figure 1

What happens if we start the shear flow? We can apply some shear stress regulated. The average shear rate may be also regulated but the local shear rate. So the increasing stress causes slow flow up to a critical stress. If the stress overrides the critical one the shear rate jumps to a higher value but not at places. The equations do not determine where the jump happens. The distribution of high shear rate regions may be

random. If the pattern of the high and low shear rate regions is fine an averaging over them is obvious. These considerations have us incline to apply a non-linear theory to give account on the average properties.

The investigation of the uniaxial load also shows interesting features. A solution

$$(9) \quad t = 2\eta\dot{d}$$

exists at any load but the analysis of the stability shows that at high load the above solution is unstable. The elongational flow collapses and rotation emerges with angular velocity perpendicular to the traction. The rate of elongation increases rapidly with increasing load. The direction of the angular velocity is not determined by the equations; the direction may be random. If the pattern of the domains of uniform rotation is fine the averaging is again obvious; a non-linear theory is again motivated.

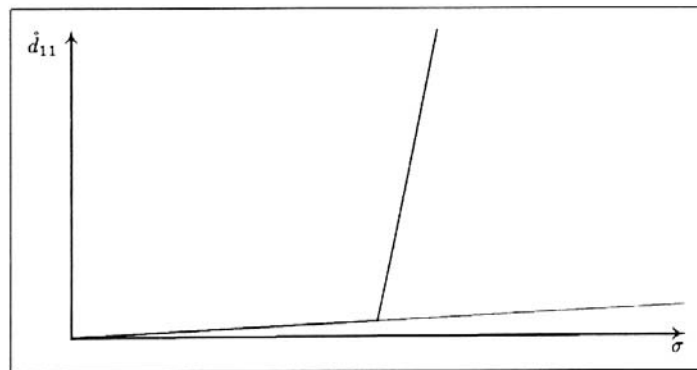


Figure 2

The rate of elongation plotted against the tension is shown in figure 2 for a material with one dynamic degree of freedom.

3. Generalized constitutive equations.

Next a non-linear theory will be presented. The model is similar the one above only the linear constitutive equations (7) are modified "slightly". The second term on the right hand side of the relaxation equations is replaced by a non-linear function.

$$(10) \quad \begin{aligned} t &= L_{00}\dot{d} - \sum_i L_{0i}\alpha_i \\ \dot{\alpha}_i &= L_{0i}\dot{d} - f_i(\alpha_i). \end{aligned}$$

The actual $f_i(\alpha_i)$ functions have to be found out. According to the traditional theories of plasticity, the f_i functions – they are isotropic functions – are taken in the form

$$f_i = \lambda_i(\alpha_i)\alpha_i,$$

where the values λ_i are scalar and depend on the invariants of the arguments. The analogy to von Mises' theory suggests that λ_i depends on the quantity $\sqrt{\alpha_i : \alpha_i}$. To arrive at a theory of plastic flow the function has to have very small value if the argument is smaller than the one belonging to the yield condition and has to increase rapidly after. The chemical reaction kinetic proposes exponential functions like

$$y = A \sinh(\chi x).$$

With extreme parameters A and χ the graph of the function looks like in figure 3. In such a case the constitutive equation for the dynamic variable α_i may be replaced by the correlation according to which $\lambda_i(\alpha_i)$ is zero if α_i is under its own yield condition and arbitrary if α_i satisfies it. One can see that the theory obtained gives the model for plastic flow. The rheological model consists of n Prandtl-Reuss element and a Newton element connected in parallel; the latter is usually

dropped (figure 4). To get this picture easier, replace the dynamic variable α_i by

$$\alpha_i = -\frac{1}{L_{0i}}t_i.$$

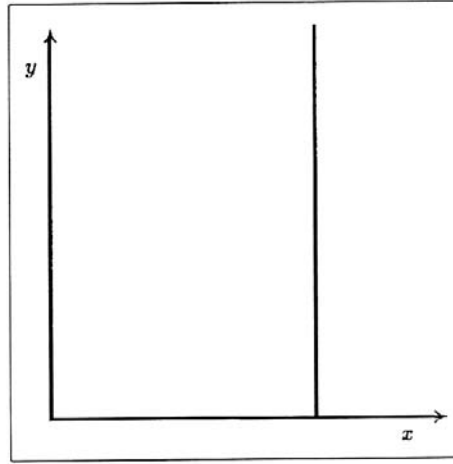


Figure 3

For the new variables, the set of the constitutive equations takes the form

$$t = L_{00}\dot{d} + \sum_i t_i$$

$$\dot{t}_i = L_{0i}^2 \dot{d} + g_i$$

where g_i is zero if t_i is under the yield condition and arbitrary if t_i satisfies it. Here the stress is split into parts. Each part has its own yield condition. If g_i is zero the part of the stress is elastic ($\dot{t}_i = L_{0i}^2 \dot{d}$); if not, the material flows. A model with sufficiently large n describes the experiments well.

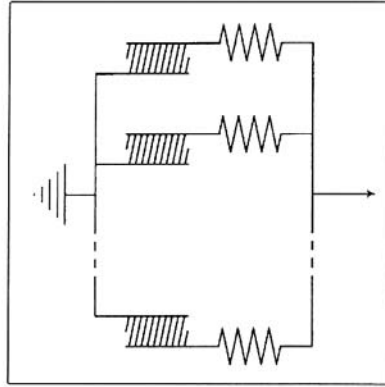


Figure 4

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